PATENT SPECIFICATION



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PROVISIONAL SPECIFICATION.



394, 325



Improvements in and relating to Sound-transmission, Soundrecording and Sound-reproducing Systems.

We, ALAN DOWER BLUMLEIN, of 57, Earl's Court Square, London, S.W. 5, a British subject, and ELECTRIC AND MUSICAL INDUSTRIES, LIMITED, of Blyth

MUSICAL INDUSTRIES, LIMITED, of Blyth 5 Road, Hayes, in the County of Middlesex, a company registered under the laws of Great Britain, do hereby declare the nature of this invention to be as follows:—

This invention relates to the transmission, recording and reproduction of sound and is more particularly directed to systems for recording and reproducing speech, music and other sound effects,
 especially when associated with picture effects in talking matrix

effects as in talking motion pictures. The fundamental object of the invention is to provide a sound recording and reproducing system whereby a true direc-20 tional impression may be conveyed to a listener thus improving the illusion that the sound is coming, and is only coming, from the artist or other sound source presented to the eye. In order that the 25 physical basis of the invention can be appreciated and the stages of its development understood, known and established facts concerning the physical relations between sound sources, sound waves 30 emitted thereby, and the human ears will be briefly summarised.

Human ability to determine the direction from which sound arrives is due to binaural hearing, the brain being able to detect differences between sounds received by the two ears from the same source and thus to determine angular direction. This function is well known and has been employed to considerable extent for

40 example in sub-aqueous directional detection in which two microphones are coninected by headphones, one to each ear of an observer, the two channels between the microphones and the two ears being 45 kept entirely separate.

45 kept entirely separate.
With two microphones correctly spaced and the two channels entirely separate it is known that this directional effect can also be obtained for example in a studio,
50 but if the channels are not kept separate (for example, by replacing the headphones by two loud speakers) the effect is largely lost. The invention contemplates con-

trolling the sound, emitted for example by such loud speakers, in such a way that 55 the directional effect will be retained.

The operation of the ears in determining the direction of a sound source is not yet fully known but it is fairly well estab-lished that the main factors having effect 60 are phase differences and intensity differences between the sounds reaching the two ears, the influence which each of these has depending upon the frequency of the sounds emitted. For low frequency sound waves there is little or no difference in intensity at the two ears but there is a marked phase difference. For a given obliquity of sound the phase difference is approximately proportional to frequency, representing a fixed time delay between 70 sound arriving at the two ears, by noting which the brain decides the direction from which the sound arrives. This operation holds for all frequencies up to that at which there is a phase difference of π . 75 radians or more between sounds arriving at the two ears from a source located on the line joining them; but above such a frequency if phase difference were the sole 80 feature relied upon for directional loca-tion there would be ambiguity in the apparent position of the source. At that stage however the head begins to become effective as a baffle and causes noticeable 85 intensity differences between the sounds reaching the two ears, and it is by noting such intensity differences that the brain determines direction of sounds at higher frequencies. It has been stated that the frequency at which the brain changes over 90 from phase- to intensity-discrimination occurs at about 700 c.p.s. but it must be understood that this may vary within quite wide limits in different circum- 95 stances and from person to person, and that in any case the transference is not sudden or discontinuous but there is considerable overlap of the two phenomena so that over a considerable frequency 100 range differences of both phase and intensity will to some extent have an effect in determining the sense of direction experienced.

From the above considerations it will 105 be clear that a directional effect is to be obtained by providing low-frequency phase differences and high-frequency intensity differences at the two ears, and it would appear that in reproducing from **5** two loud speakers the differences received by two microphones suitably spaced to represent human ears would give this effect to a listener if each microphone were connected only to one loud speaker.

- 10 It can be shown however that phase differences necessary at the ears for low-frequency directional sensation are not produced by phase differences at two loud speakers (both of which communicate
 15 with both ears) but are produced by intensity differences at the speakers:
- while initial intensity differences from the sources necessary for high-frequencies are not sufficiently marked when the sounds
- 20 reach the ears, and to produce suitable effects therefore the initial differences must be amplified.

It will be seen therefore that the invention consists broadly in so controlling the

- 25 intensities of sound to be or being, emitted by a plurality of loud speakers or similar sound sources, in suitable spaced relationship to the listener, that the listener's ears will note low-frequency phase differences
- 30 and high-frequency intensity differences suitable for conveying to the brain a desired sense of direction of the sound origin.
- It must be understood that the control-35 ling of intensities of a plurality of loud speakers spaced, for example, round a motion picture screen has previously been proposed and no novelty for mere intensity control per se is claimed, except inso-
- '40 far as the nature of the control is such as to provide the necessary phase and intensity difference sensations. If the sound is first recorded and subsequently reproduced from the records, the control may '25 he wholly effected either during the
- 45 be wholly effected either during the recording or during reproduction, or may be partially carried out in each stage. More specifically the invention consists

in a method of transmitting, recording 50 and/or reproducing sound wherein a

- plurality of transmission channels so interact, each upon each, or are in such relation or so relatively modified in combination and subsequently reseparated, 55 that the complete intelligence initially
 - transmitted is further conveyed, differently arranged, between the channels.

The invention also consists in a method of transmitting, recording and/or repro-60 ducing sound wherein phase differences between a plurality of signals are con-

verted into amplitude differences.

The invention also consists in apparatus and means for carrying into effect the 65 above specified methods of sound trans-

mission, recording and/or reproduction, and in further features which will become apparent from the following description of one manner of carrying out the invention. It must be understood however that 70 this description is given merely by way of example and does not impose any restrictions upon the scope of the invention or the manner and means whereby it may be accomplished 75

It will be clear that the invention is particularly applicable to talking motion pictures and the following description will therefore be given with reference to this application. In one form of the invention convenient for this purpose the sounds to be recorded and reproduced with the pictures may be received by two pressure microphones mounted on opposite sides of a block of wood to represent ears -85 on an artificial head. The outputs from the two microphones are taken to suitably arranged transformers or bridge or network circuits which convert the two primary channels into two secondary channels which may be called the sum-90 mation and difference channels. These are arranged so that the current flowing into the summation channel will represent half the sum, or the 05 mean, of the currents flowing n the two original channels, while the current flowing into the difference channel will represent half the difference of the currents in the original channels. If 100 the original currents differ in phase only, the current in the difference channel will

be $\frac{\pi}{2}$ different in phase from the current

in the summation channel. This difference current is then passed through a 105 condenser; the voltage across this condenser will be in phase with the summation channel current. By passing the summation channel current through a resistance, a voltage is obtained which 110 remains in phase with the voltage across the condenser in the difference channel. These two voltages are then combined and re-separated by the same process as previously adopted so as to produce two final 112 channels. The voltage in the first final channel will be the sum of these voltages and the voltage in the second final channel will be the difference between these voltages. Since these voltages were in phase 120 the two final channels will be in phase but will differ in magnitude. By choosing the value of the shunt resistance in the summation channel and the shunt condenser in the difference channel for a 126 given frequency, any degree of amplitude difference in the final channel can be obtained for a given phase difference in the original channels. For the low fre-

quencies it can be shown that the phase difference between the waves will, for a given obliquity of the sound source, vary proportionately with frequency, being very small for a very low frequency. Hence the use of a shunt condenser in the difference circuit will have the effect of producing a fixed intensity difference in the final channels for a given obliquity

10 at all low frequencies. For the higher frequencies as indicated above it is not necessary to convert phase shifts into amplitude differences, but simply to modify amplitude differences.

- **15** The shunt condenser in the difference circuit is therefore built out with a resistance whose value determines the degree of modification.
- It may be found necessary to employ 20 more complex circuits than the shunt resistance and condenser in the summation circuit and shunt resistance in the difference circuit, which however form the basic arrangement. However it must be 25 understood that the circuits employed may be considerably modified as required

without departing from the scope of the invention. If two very small microphones are used

30 and placed very close together it may be found possible to obtain microphone outputs which do not differ appreciably in amplitude but only in phase for all working frequencies. In this case the modi35 fying circuit would be arranged to convert phase differences into amplitude differences throughout the entire frequency range. The phase differences dealt with at the low-frequencies however
40 may be so small that in this case slight differences in the two microphone circuits would have very large effects. On this account microphone spacing of the same order as that of the human ears is most
45 suitable.

The impulses transmitted through the two channels as indicated above may then be recorded on two sound tracks on a film, for example, by any suitable or known 50 means, which record may comprise a sound track of constant density and variable width (e.g. an oscillograph record), or a sound track of constant width and variable density (e.g a Kerr cell record). Such a record may be reproduced by 55 passing light from the same slit through the two tracks. separating the beam into the two record portions by means of prisms or like optical means and employ-60 ing the outputs from two photo-electric cells, excited by these separate parts of the beam (after amplification) to operate two loud speakers disposed one on each side of the screen upon which the cinema-.65 tograph pictures are projected.

It will be appreciated that the amount of modification of the impulses transmitted through the summation and difference channels as indicated above depends upon a number of factors, including the 70relative spacing of the microphones and of the loud speakers, and the size and positioning of the screen. It can be shown that for low frequencies ω the degree of modification required in the 75difference channel as compared with the modification in the summation channel is given by:—

$$\mathrm{K}=rac{2v}{j\omega}~.~rac{y}{ heta k}~.~rac{s}{x}$$

v = velocity of sound.

where

- y = fraction of half picture film width which the image of the sound source is off centre.
- θ = angle of obliquity, in radians, of the 85 source from the median plane between the microphones.
- k = effective distance a part of the micro-phones.
- s = width of screen of theatre. x = distance apart of loud speakers in

theatre. This expression in effect gives the impedance of the shunt capacity in the difference channel in terms of the resistance in the summation channel. It holds for all frequencies where k is small compared to the wavelength, and is based on the assumption that the θ is small and that x and s are small compared with the listener from the screen and loud speakers.

The portion
$$-\frac{g}{\Theta L}$$
 is a factor of the

recording, and is constant for a given arrangement if either the camera is in 105 line with the microphones and the centre of the picture, or the action does not move appreciably to or from the microphones and camera. When recording, the relative distances of camera and microphones **110** and the focal length of the lens may be adjusted to maintain this factor a constant.

The expression
$$\frac{\delta}{m}$$
 is a constant for the

theatre. As regards low frequencies only, 115 the distance apart of the speakers need not exceed the screen width, but should certainly not be closer than 70% of the screen width. The closer the loud speakers the greater the necessary power 120 handling capacity, but the less the troubles introduced by formation of stationary waves.

For the high frequencies no definite expression can easily be obtained, and the 125 modification used will probably have to

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be gauged empirically by trial and error. The arguments and formula given above are based on a direct wave analysis and may have to be considerably modified in **b** order to allow for reflection or other acoustic effects. It is preferred therefore to introduce the modifications it is

proposed to employ, at the theatre since all factors will then enter into considera-10 tion. It will be clear that, as indicated above, the modifying networks and channel arrangements may be employed

- between the microphones and the film during recording, or between the record 15 and the loud speakers during reproduction, and the latter course, in addition to allowing of adjustment of the arrangements to suit the particular theatre as indicated above, has the additional
- 20 advantage that the sound film can be reproduced by a single reproducing head or channel if for example one of the dual arrangements breaks down, or in a theatre which, having one installation, does not 25 wish to go to the expense of installing a

second apparatus.

In order to employ successfully a system of the kind described above it is necessary to carry out preliminary experiments

- 30 to determine the most suitable value of modification to be employed for each recording, and it is also necessary to standardise various factors entering into every recording. In the preliminary
- **35** experiments, before recording, volume indicator measurements may be made with a standard source placed at the extremes of the "set", i.e. the space within which recording is to be effected, and from these
- **40** the proposed modifying network laid out. A further experiment may also be effected to standardise phase angles on the film. At the theatre a simple adjustment may be provided to check and balance the input
- 45 to the two channels, a length of test film being used for this purpose. It will thus be seen that the total theatre equipment necessary is very simple and consists in a transmission modifier (comprising two
- 50 or four transformers, for example, artificial line resistances and the control network, which may be no more than a condenser and a resistance) and two normal sound-reproducing heads or pick-ups, or

55 one specially designed head or pick-up adapted to separate the two recordings to two complete reproducing channels. There is no reason why the second channel used should not be the "stand-by"
60 channel now often installed for safety

60 channel now often installed for safety since if, as indicated above, one of the channels breaks down reproduction may be continued without serious consequences on the other channel only.

65 In connection with the standardisation

indicated above, while the binaural "transfer" frequency (from phase- to intensity-discrimination) need have no definite significance in recording, since it is a function of the human brain it is nevertheless necessary to fix a changeover frequency from high- to low-frequency working for recording, since this frequency fixes the form of modification to be used, the distance apart of the microphones and the form of baffie convenient between them. Any frequency may be chosen as standard after experience has decided which is most suitable. Instead of standardising it may be possible from the preliminary experiments to allow electrically for variation of microphone positions and/or of microphone spacing (although the latter would be extremely difficult) and it must be understood that this arrangement falls within the scope of the invention.

The above described system is based upon considerations in which no account is taken of sound reflections or interference either during recording or reproduction. If difficulties arise from this cause they may be overcome by employing a second pair of loud speakers differently spaced and having a different modifying network from the first pair: or a row of speakers may be used with a composite, progressive modifying network to supply them: or the two speakers may be placed comparatively close together, no direc- # tional effect in this case being given to high frequencies, except insofar as a phase difference (when the angle of obliquity of the sound varies only within such very small limits as to avoid g ambiguous results) may be employed to give some such effect even at high frequencies.

The system so far described employs to receive the sound waves two pressure <u>1</u> microphones. Velocity or moving conductor microphones (e.g. moving strip microphones) are also very suitable and may be employed, in which case various alterations in the system may be necessary. Such velocity microphones give a response varying as the cosine of the angle of incidence of the sound relativeto the direction of normal or optimum incidence, and they have the advantage <u>1</u> in the present system that a specific degree of loud speaker output separation may be obtained without phase-conversion or like network modifications.

Three general arrangements employing velocity microphones are possible, and in all cases the microphones are placed as near together as possible instead of being spaced as artificial ears, as in the case of pressure microphones.

(1) Two velocity microphones are placed one with its axis directly facing in the direction of the centre of the scene, and the other with its axis at right angles to
5 that direction. A performer speaking from the middle of the scene will affect only the face-on microphone, but if he moves to one side both microphones will provide outputs, while if he moves the

- 10 other way the outputs are identical but the phase of the edge-on microphone is reversed. Since the microphones are close together no phase differences are experienced between them and if their
 15 outputs are summed and differenced after a suitable amount of relative amplification the two final channels differ in magniiude in the correct manner for operating
- the loud speakers to give the desired direc20 tional effect. Such sum and difference arrangement differs from the modifying network employed with pressure microphones in that the pressure type provide phase differences (whereby direction is
 25 determined) which have to be converted, whereas with the velocity type the edge-on microphone provides an output proportional to the obliquity of the source.
- (2) Two velocity microphones may be
 30 placed with their axes perpendicular to one another and each axis at 45° to the direction of the centre of the screen. They are sufficiently close together to render phase differences of the outputs
 35 negligible and the output amplitudes differ approximately proportionally to the obliquity of the incident sound. They may therefore be amplified similarly, and supplied directly to the loud speakers to
 40 which they will give the correct amplitude differences for the desired directional effect provided the relationship between the various dimensions of the recording

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- the various dimensions of the recording and reproducing "lay-outs" are correct.
 45 If it is desired to accommodate any differencies between the "lay-outs" the outputs may be modified by networks, in the manner described, suitably to increase or decrease the differences between them.
- 50 (3) Two microphones may be arranged, with the two axes lying symmetrically to the direction of the centre of the screen and with an angle between them of say θ degrees, so that sound from a performer
- 55 at the centre subtends an angle of $\frac{0}{2}$
- degrees to each microphone. If θ is small a small movement of the performer to one side is sufficient to make one microphone "edge-on" and to reduce its output to zero, while if θ is large a large movement of the performer is necessary to do this. By making θ adjustable different "lay-outs" may be accommodated without the modification indicated under (2)

and it will be clear also that this pro-65 vides a method of directional sound transmitting, recording and reproduction which avoids the necessity of combining and reseparating the two channels.

Two velocity microphones set with their 70 axes symmetrically inclined to the direction of the centre line of the scene, may if placed one above the other, be employed also to provide significance of vertical as well as horizontal movement of the sound 75 source. Such vertical displacement of the source will in this arrangement give phase differences to the outputs while lateral displacement gives amplitude differences, and these can be separated, the phase differences converted to inten-80 sity differences by modifying networks, as described, and the resulting impulses employed to operate four or more loud speakers distributed round the screen, the 85 transmission occupying however only two channels. A similar effect may be obtained with a plurality of pressure microphones by employing suitable modification previous to transmission. 90

In obtaining a complete directional "sound picture", i.e. both horizontal and vertical directional effects, the invention is not limited solely to the use of two microphones. A plurality may be employed and their outputs suitably 95 collected and/or $\mathbf{modified}$ and/or separated to transmit suitable differences of impulses to a plurality of loud speakers. The general feature is that two trans- 100 mitting channels, receiving impulses from two or more microphones for example, communicate two directional senses at right angles to one another, the sounds whereby this is done being provided by a 105 plurality of loud speakers. It will be seen that while with pressure

It will be seen that while with pressure microphones it is preferred to transmit phase differences rather than amplitude differences and convert from one to the 110 other in the last stage, with velocity microphones it is more convenient to transmit the two channels in phase but at different amplitudes, the only modification then necessary being an increase or 115 decrease of the amplitude differences should the reproducing "lay-out" differ from the recording "lay-out" or should more than two loud speaker positions be used.

There is a simple method by which modifications for increase or decrease of differences between channels may be effected if no conversion of phase differences into amplitude differences is required. The method is particularly useful for the operation of more than two loud speakers. If the transmission is effected in the form of two channels of

similar phase but different amplitudes, an alteration of these amplitude differences may be effected by connecting one wire of each channel together and connecting 5 a choke between the other two wires of the two channels. The outgoing channels whose difference is to be a modification of the original difference, are connected to the common point of the original

10 channels, and to tappings along the choke. If the differences are to be increased, the tappings at which the output channels are connected lie outside the tappings to which the input channels are connected,

15 so that the choke operates in effect as an auto-transformer amplifying the differ-ence voltages. Similarly, for a reduction of differences, the output channels are tapped intermediately between the two 20 input channels. Modifications of this

arrangement in which the devices are balanced about earth, etc. may be arranged, but the chief advantage is that the modification is varied entirely by 25 altering tappings along a transformer or choke, and that no great power loss is involved.

This arrangement of a choke or transformer is well suited to working a number 30 of loud speakers for binaural reproduction. In this case, the two outputs from power valves are fitted to a choke along which the loud speakers are tapped. The

position of the loud speaker tappings can 35 be adjusted to suit their relative positions, and it can be arranged that the valves are working into their best impedances. Transformers may be used to ensure the speakers taking their correct fraction of 40 the output.

While, in connection with the above described systems, it is suggested that when it is desired to record the sounds for subsequent reproduction this may be

45 done upon a film, the invention is not limited to that medium since the recording may if desired be effected on discs or cylinders of suitable material. In carrying out the invention in this manner the

- 50 two channels may if desired be recorded in separate grooves but it is preferred that they be recorded in the same groove having a hill and dale and also a lateral cut movement. For the purposes of television 55 previous proposals have been made
- whereby a wax disc has a sound record as a hill and dale cut and a picture record as a laterally cut V-shaped groove at the bottom of the hill and dale groove, or vice 60 versa. Such records appear unsuited for
- separate and distinct sound recordings since undoubtedly considerable cross-talk between the two recordings would occur. They can however be used for two 65 channels of the kind contemplated in the

present invention, one being only slightly different from the other, since a certain amount of cross-talk in this case does not matter, or can be allowed for. Furthermore, the records now proposed are dis-10 tinguished from those previously known in that both channels may separately be recorded in one groove by a single recording tool (either of moving iron or mov-75 ing coil type) and be reproduced therefrom by a single reproducing device or pick-up.

If the two channels being recorded are directly picked up from two micro-phones, or are intended to work unmodi-2.5 fied into two speakers, that is with intensities and qualities similar, it is preferred not to cut one track as lateral cut and the other as hill and dale, but to cut them as two tracks whose movement axes lie at S. 45° to the wax surface, or at some other convenient angle dependent on the relative available intensities from lateral cut and hill and dale respectively. If, however, the two channels recorded are such as summation and difference channels, it is preferred to separate them completely into pure hill and dale and pure lateral cut, i.e. to make the recording axes normal and tangential to the wax surface.

The result in the two above suggested cases is very similar since channels recorded at 45° to the wax surface give their sum and difference as the effective lateral and hill and dale amplitudes. 100

It will be appreciated that a record, cut as a combined hill and dale and lateral, may be reproduced if desired as two skew direction cuts, the basic principle being that the groove has ampli- 105 tude in any direction in the plane at right angles to the direction of wax movement, and the recording and reproducing directions may be chosen as any pair of axes lines, not necessarily at right angles in 110 this plane.

It would appear that for such a record, a material other than that now used for lateral cut records, would be desirable, and a material of the nature of cellulose 115 acetate is indicated.

The track section is preferably adapted to work with a sapphire and have a suffi-ciently fine angle to give lateral as well as vertical control to the sapphire.

The recorder whereby both channels may be cut by a single tool on the same groove may take various forms, the underlying feature being that a light stylus is pulled in two directions at right angles to use another and each preferably at 45° to the wax surface.

In one such form the recorder may consist in a short circular reed mounted close above and parallel with the wax track. 130

One end of this reed may be firmly fixed like manner any axis conversion can be in the one pole of an electromagnet which would pass back over it and complete the magnetic circuit in two laminated arms 5 extending down towards the other free end of the reed. These arms form two poles adjacent to a square portion of the reed at its free end, each pole being adapted to pull the reed in a direction at 10 45° to the wax surface. The reed may he suitably damped, e.g. with rubber, and have a resonant frequency at the top of, or above, the working range. The free end of the reed carries the sapphire. The 15 two pole pieces may be wound with speech coils, and the energisation of one of these would move the sapphire in an upward direction at 45° to the wax surface. Any reduction in the pull of one 20 pole due to the increased flux of the other, may be compensated by additional windings on one pole connected in series

with those on the other. Thus energising any winding will produce the required 25 movement at 45° to the wax surface, the characteristic being equalised. An alternative moving coil design employing electromagnetic damping may consist of a moving member in the shape 30 of a T. The lower arm of the T extends

towards the wax and carries the sapphire; the horizontal member of the T is at right angles to the direction of wax movement, and carries at its ends two wound mov-35 ing coils. These moving coils whose axes are vertical move in suitable annular fieldgaps. The movement may be supported at approximately the centre of the T by elastic means, which permit of both rota-40 tional and vertical movement within the plane of the T. Adjustments may be plane of the T. Adjustments may be provided to make the resonant frequency The of these two movements similar. characteristic correction for each coil 45 drive may be similar to those used for the

moving coil sound recorder described in the specification of British Patent No. 350,998.

Energisation of one coil both rotates 50 and translates the T member giving an inclined cutting direction. By suitably proportioning the length of the vertical member of the **T** this axis can be placed where desired, and further can also be 55 controlled by interconnecting portions of

the coil windings. In all the devices described above, the angles of the axes can be altered by suitably connecting the speech windings; for 60 instance, axes which are normally inclined at 45° to the wax surface can be converted into pure hill and dale and lateral cut axes by arranging that the speech windings are in series aiding for one channel

effected by suitably combining the channels through transformers.

In designing an electric pick-up to reproduce both channels care must be 70 taken that the inertia is kept as low as possible, and with this in mind a very light replica of the above described mov-Alternatively, a moving system in the form of a T following the lines of the moving coil recorder suggested above, 75 may be employed; moving coils may be used for such a pick-up or the coils replaced by air gaps of an iron system. 80 Since the fundamental resonant frequency of a pick-up appears to be of no critical importance as regards its characteristic, it may not be necessary to adjust the resonant frequency in the two modes to 85 the same value, which would simplify the design. Adjustments for sensitivity in the two modes could be made by suitably connecting coils wound on the two limbs of the magnetic circuits. 90

The hereindescribed acoustic system while being especially applicable to talking pictures is not limited to such use. It may be employed in recording sound quite independently of any picture effects 95 and in this connection (as well as when used in cinematograph work) it seems probable that the binaural effect introduced will be found to improve the acoustic properties of recording studios 100 and to save any drastic acoustic treat-ment thereof while providing much more realistic and satisfactory reproduction. Furthermore, the system may clearly be employed when the microphone outputs 10 are led directly to the loud speakers instead first of being recorded, and such an arrangement may for example be employed in public address systems in which directional sound effects are desired. 110 In general the invention is applicable in all cases where it is desired to give directional effects to emitted sound. Also in all cases, both when the impulses are fed directly to the loud speakers and when 115 they are recorded for subsequent reproduction the total modification and/or interaction of the channels may be accomplished in more than one stage. For example, using pressure microphones, the 120 low frequency phase differences may be amplified, the medium frequency phase differences converted to amplitude differences, and the high frequency amplitude differences augmented in a first stage of 125 modification; the low frequency phase differences may then be converted to amplitude differences in a later stage of modification. One or both of these stages 63 and opposing for the other channel. In may occur either before or after the 130

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sound has been recorded. In this manner the very small low frequency phase differences are augmented before they are amplified, so avoiding troubles due to 5 small low frequency phase shifts in amplifiers.

Moreover, the various devices employed for carrying the invention into effect must be understood not to be limited to their

10 use with the other devices also hereindescribed since clearly many parts, such, for example, as the dual track record prepared by a single cutter, and the multistrip direction-detecting microphone, are 15 clearly of wide use separately of one another. Such uses fall within the scope of this invention.

It must finally be understood that the invention is not restricted solely to the details of arrangements of the forms of 20 the invention described above since various modifications may be introduced in order to carry the invention into effect under different conditions and requirements which have to be fulfilled without 25 departing in any way from the scope covered thereby.

Dated this 14th day of December 1931. MARKS & CLERK.

COMPLETE SPECIFICATION.

Improvements in and relating to Sound-transmission, Soundrecording and Sound-reproducing Systems.

We, ALAN DOWER BLUMLEIN, of 57, Earl's Court Square, London, S.W. 5, a 30 British subject, and ELECTRIC AND. MUSICAL INDUSTRIES, LIMITED, of Blyth Road, Hayes, in the County of Middlesex, a company registered under the laws of Great Britain, do hereby declare the 35 nature of this invention and in what manner the same is to be performed, to be particularly described and ascertained in and by the following statement :--

- This invention relates to the 'trans-40 mission, recording and reproduction of sound and is more particularly directed to systems for recording and reproducing speech, music and other sound effects. It is applicable in particular, although not
- 25 exclusively, to systems associated with picture effects as in talking motion pictures.

The fundamental object of the invention is to provide a sound recording, re-

- 50 producing and/or transmission system whereby there is conveyed to the listener a realistic impression that the intelligence is being communicated to him over two acoustic paths in the same manner as he
- 55 experiences in listening to everyday acoustic intercourse and this object embraces also the idea of conveying to the listener a true directional impression and thus, in the case in which the sound is
- 60 associated with picture effects improving the illusion that the sound is coming, and is only coming, from the artist or other sound source presented to the eye.
- The invention is not, however, limited 65 to use in connection with picture effects, but may, for example, be used for improving the qualities of public address, telephone or radio transmission systems, or for improving the quality of sound 70 recordings. When recording music con4-1

siderable trouble is experienced with the unpleasant effects produced by echoes which in the normal way would not be noticed by anyone listening in the room 75 in which the performance is taking place. An observer in the room is listening with two ears, so that echoes reach him with the directional significance which he associates with the music performed in such a room. He therefore discounts these 80 echoes and psychologically focuses his attention on the source of sound. When the music is reproduced through a single channel the echoes arrive from the same direction as the direct sound so that con-85 fusion results. It is a subsidiary object of this invention so to give directional significance to the sounds that when reproduced the echoes are perceived as such.

In order that the physical basis of the invention can be appreciated and the stages of its development understood, known and established facts concerning the physical relations between sound sources, sound waves emitted thereby, and the human ears will be briefly summarised.

Human ability to determine the direction from which sound arrives is due to 100 binaural hearing, the brain being able to detect differences between sounds received by the two ears from the same source and ⁴ thus to determine angular directions from which various sounds arrive. This function is well known and has been employed ¹⁰⁵ to considerable extent for example in subaqueous directional detection in which two microphones are connected by headphones, one to each ear of an observer, the two channels between the microphones 110 and the two ears being kept entirely separate.

With two microphones correctly spaced

and the two channels kept entirely separate e.g. by using headphones it is known that this directional effect can also be obtained for example in a studio. If, 5 however, the channels are not kept

- separate (as, for example is the case in previously proposed arrangements for recording and/or reproducing sound, in which sounds picked up by a plurality of
- 10 pressure microphones are led to loud speakers which take the place of the headphones) the effect is almost entirely lost and such systems have therefore not come into common use since they are quite un-
- 15 satisfactory for the purpose. The present invention contemplates controlling the sound, emitted for example by such loud speakers, in such a way that the directional effect will be retained.

The operation of the ears in determin-20 ing the direction of a sound source is not yet fully known but it is fairly well established that the main factors having effect are phase differences and intensity differences between the sounds reaching the two ears, the influence which each of these has depending upon the frequency of the sounds emitted. For low frequency sound waves there is little or no difference 30 in intensity at the two ears but there is a marked phase difference. For a given obliquity of sound the phase difference is approximately proportional to frequency, representing a fixed time delay between 35 sound arriving at the two ears, by noting which the brain decides the direction from which the sound arrives. This operation holds for all frequencies up to that at which there is a phase difference of π 40 radians or more between sounds arriving at the two ears from a source located on the line joining them; but above such a frequency if phase difference were the sole feature relied upon for directional loca-45 tion there would be ambiguity in the apparent position of the source. At that stage however the head begins to become

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intensity differences between the sounds 50 reaching the two ears, and it is by noting such intensity differences that the brain determines direction of sounds at higher frequencies. It has been stated that the frequency at which the brain changes over 55 from phase- to intensity-discrimination occurs at about 700 c.p.s, but it must be understood that this may vary within quite wide limits in different circumstances and from person to person, and 60 that in any case the transference is not sudden or discontinuous but there is considerable overlap of the two phenomena so that over a considerable frequency

effective as a baffle and causes noticeable

range differences of both phase and in-65 tensity will to some extent have an effect

in determining the sense of direction experienced.

From the above considerations it will be clear that a directional effect is to be obtained by providing impressions at the two ears of low frequency phase differences and high frequency intensity differences, and it would appear that in reproducing from two loud speakers the differences received by two microphones suitably spaced to represent human ears would give 75 this effect to a listener if each microphone were connected only to one loud speaker. It can be shown however that phase differences necessary at the ears for low 80 frequency directional sensation are not produced solely by phase differences at two loud speakers (both of which com-municate with both ears) but that intensity differences at the speakers are 85 necessary to give an effect of phase difference : while initial intensity differences from the sources necessary for high frequencies are not sufficiently marked when the sounds reach the ears, 90 and to produce suitable effects therefore the initial intensity differences must be amplified. It is for this reason that the aforementioned methods previously proposed (wherein only pressure microphones **9**5 were used) are not successful in achieving the desired effect, these necessary alterations not having been understood or in any way attained in those prior arrangements.

It will be seen therefore that the invention consists broadly in so controlling the intensities of sound to be, or being, emitted by a plurality of loud speakers or similar sound sources, in suitable spaced 105 relationship to the listener, that the listener's ears will note low frequency phase differences and high frequency intensity differences suitable for conveying to the brain a desired sense of direction 110 of the sound origin. In other words the direction from which the sound arrives at the microphones determines the characteristics (more especially, as will become apparent hereafter, the intensities) of the 115 sounds emitted by the loud speakers in such a way as to provide this directional sensation.

It must be understood that the manual control by an observer of intensities of a 420 plurality of loud speakers spaced round a motion picture screen has previously been proposed but this method suffers considerably from the defects indicated above, and in any case is very difficult and incon-venient to operate. No novelty for mere intensity control per se is however claimed, except insofar as the nature of the control is such as to provide the necessary relative phase and intensity 130

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difference sensations.

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If in accordance with the invention the sound is first recorded and subsequently reproduced from the records, the control 5 may be wholly effected either during the recording or during reproduction, or may be partially carried out in each stage. It

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m must}$ be understood \mathbf{that} wherever throughout this specification the words 10 "sound transmission" are employed (more especially in the claims specified below), they cover (unless the context -otherwise requires) not only the case in

- which impulses pass directly from the 15 microphones to the loud speakers, but also those arrangements embodying an intermediate process or system of recording; and in the latter cases the said words apply to either, or both, the passage of
- 20 impulses from the microphones to the recording system, and from the reproducer to the loud speakers.

More specifically the invention consists in a system of sound transmission wherein

- 25 the sound is picked up by a plurality of microphone elements and reproduced by a plurality of loud speakers, comprising two or more directionally sensitive microphones and/or an arrangement of elements
- 30 in the transmission circuit or circuts whereby the relative loudness of the loud speakers is made dependent upon the direction from which the sounds arrive at the microphones.

35 The invention also consists in a system of sound transmission wherein the sound is received by two or more microphones, wherein at low frequencies difference in the phase of sound pressure at the micro-40 phone is reproduced as difference in

volume at the loud speakers. The invention further consists in a system of sound transmission in which the original sound is detected by two or more 45 microphones of a type such as velocity microphones whose sensitivity varies with the direction of incident sound, and in which the dependence of the relative responses of the microphones to the direc-

50 tion of an incident sound wave is used to control the relative volumes of sound emitted by two or more loud speakers.

The invention also consists in a system of sound transmission wherein impulses 55 from two microphones transmitted over individual channels are adapted to interact whereby two sets of impulses are further transmitted consisting in half the

sum and half the difference respectively 60 of the original impulses, said impulses being thereafter modified to control the relative loudness of loud speakers whereby the sound is to be reproduced.

The invention also consists in a system 65 of sound transmission wherein the sound

is picked up by two directionally sensitive microphones which are so spaced and/or with their axes of maximum sensitivity so directed relative to one another and to the sound source, that the relative loud-26 ness of loudspeakers which reproduce the impulses is controlled by the direction from which the sound reaches the microphones.

The invention also consists in a system 17 as set forth above wherein two sets of impulses are mechanically recorded in the same groove.

The invention also consists in a system as set forth above wherein the impulses are 8. transmitted by madio telephony.

The invention also consists in a system as set forth above in combination with means for the photographic recording or transmission and/or reproduction of pictures.

The word channel, as employed herein, means an electric circuit carrying a current having a definite form depending upon the original sounds in the studio. 90 Thus two channels may be different not only because the average intensities or types of current in them differ but also because they originate from two microphones in different positions in the studio. 93

The nature of the invention will become apparent from the following description of various methods and modes of carrying it into effect but it must be understood that the different forms described are 100 given merely by way of example and do not impose any restrictions upon the scope of the invention or the manner and means whereby it may be accomplished.

The description will be more readily 100 understood by reference to the accompanying drawings, wherein

Figure 1 represents diagrammatically the assembly of one system according to 410 the invention ;

Figure 2 represents a microphonic arrangement for use according to one form of the invention:

Figure 3 represents a transformer arrangement employed in one form of the 113 invention : and

Figure 4 shows a symbolic representation of the arrangement shown in Figure 3.

Figures 5, 6 and 7 represent various 120 circuit arrangements applicable to various forms of the invention, while

Figures 8. 9, 10 and 11 represent different forms of sound recorders which may be employed.

It will be clear that the invention is particularly applicable to talking motion pictures and the following description will therefore be given with reference to this application. In one form of the in- 190

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vention convenient for this purpose shown in Figure 1 the sounds to be recorded and reproduced with the pictures may be received from a source a by two pressure 5 microphones a_1 , a_2 mounted on opposite

- sides of a block of wood or baffle b which serves to provide the high frequency intensity differences at the microphones in the same way as the human head operates 10 upon the ears as indicated above. The
 - outputs from the two microphones are after separate amplification by separate similar amplifiers b_1 , b_2 taken to suitably arrange circuits c comprising transformers
- or bridge or network circuits which con-15 vert the two primary channels into two secondary channels which may be called the summation and difference channels. These are arranged so that the current
- 20 flowing into the summation channel will represent half the sum, or the mean, of the currents flowing in the two original channels, while the current flowing into the difference channel will represent half 25 the difference of the currents in the original channels.

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One convenient transformer arrangement for this purpose is shown in Figure 3 wherein input currents from amplifiers 30 b_1 , b_2 are separately fed each to two primary windings, one on each of two transformers, the secondary winding of each transformer providing a "sum" or "difference" output curvent on account 35 of the senses in which the primary coils are wound as shown. A diagrammatic representation of a sum and difference arrangement (which may consist of a transformer similar to that of Figure 3 or 40 any other suitable arrangement of circuit elements) is shown in Figure 4.

In accordance with the form of the invention being described the two outputs from the sum and difference arrangement 45 are modified in order to obtain subsequently the desired sound effects and one convenient circuit arrangement for effecting this is shown in Figure 5 which represents the portion of the circuits indicated by c in Figure 1. Assuming the original currents differ in phase only, the current in the difference channel will

be $\frac{\pi}{2}$ different in phase from the current

in the summation channel. This 55 difference current is passed through two resistances d and e in series between which a condenser f forms a shunt arm. The voltage across this condenser f will be in phase with that in the summation channel. By passing the current in the 60 summation channel through a plain resistive attenuator network composed of series resistances g, h and a shunt resistance i, a voltage is obtained which remains in

phase with the voltage across the con-65 denser f in the difference channel. These two voltages are then combined and reseparated by a sum and difference process such as previously adopted so as to pro-duce two final channels. The voltage in 70 the first final channel will be the sum of these voltages and the voltage in the second final channel will be the difference between these voltages. Since these voltages were in phase the two final 75 channels will be in phase but will differ in magnitude. By choosing the value of the shunt resistance i in the summation channel and the shunt condenser f in the difference channel for a given frequency, any degree of amplitude difference in the 80 final channels can be obtained for a given phase difference in the original channels. For the low frequencies it can be shown that the phase difference between the waves will, for a given obliquity of the 85 sound source, vary proportionately with frequency, being very small for a very low frequency. Thus for a given obliquity of the sound the current in the difference 90 channel will be increasingly great compared with that in the summation channel the higher the frequency. Hence the use of a shunt condenser f in the difference circuit will have the effect of producing a 95 fixed intensity difference in the final channels for a given obliquity at all low frequencies.

For the higher frequencies as indicated above it is not necessary to convert phase 100 shifts into amplitude differences, but simply to reproduce amplitude differences. The shunt condenser f in the difference circuit is therefore built out with a resistance k whose value is substantially equal $_{105}$ to that of resistance i.

In building this circuit the capacity of the condenser f is of such value that its impedance is small compared with that of the series resistances d and e over the 110 whole working range, while the value of resistance k is such that it equals the reactance of the condenser at approximately the frequency above which it is desired not to convert phase differences 115 into amplitude differences. The value of kis in general equal to that of i, in which case the amplitude differences for high frequencies are passed on without modification.

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It may be found necessary to employ more complex circuits than the shunt resistance k and condenser f in the difference circuit and shunt resistance iin the summation circuit, which however 125 form the basic arrangement. However it must be understood that the circuits employed may be considerably modified as required without departing from the scope

of the invention.

The outputs from the modifying circuit (Figure 1) are passed to amplifiers d_1 , С d_2 and thence to loud speakers e_1, e_2 suit-5 ably disposed on each side of a picture screen. It is to be understood that Figure 1 merely traces the passage of intelligence from the source a to a recipient and no recording or reproducing system has 10 been shown. Such may however be inserted anywhere along the electrical circuit such for example as between amplifiers b_1 , b_2 and modifying assembly c, or between assembly c and amplifiers

15 d_1, d_2 . In the latter case the impulses transdicated above may for example be recorded on two sound tracks on a film

20 by any suitable or known means, each of which records may comprise either a sound track of constant density and variable width (e.g. an oscillograph record), or a sound track of constant width and 25 variable density (e.g. a light valverecord). Alternatively both records may be made

on a single track comprising a combination of the variable width and variable density forms of recording.

Such a record may be reproduced by 30 passing light from the same slit through the two tracks, separating the beam into the two record portions by means of prisms or like optical means and employ-35 ing the outputs from two photo-electric

cells, excited by these separate parts of the beam (after amplification) to operate two loud speakers disposed one on each side of the screen upon which the cinematograph pictures are projected. 40

From the above description it will be clear that obliquity of the direction of sound wave propagation relative to the microphones a_1, a_2 will produce differences

45 of intensity at the loud speakers so as to give an impression to an observer of oblique sound incidence.

If two very small microphones are used and placed very close together it may be

- 50 found possible to obtain microphone outputs which do not differ appreciably in amplitude but only in phase for all working frequencies. In this case the the modifying circuit may be arranged to
- 55 convert phase differences into amplitude differences throughout the entire fre-quency range. The phase differences dealt with at the low-frequencies however may be so small that in this case slight
- 60 differences in the two microphone circuits would have very large effects. On this account microphone spacing of the same order as that of the human ears is most suitable.

65 It will be appreciated that the amount

of modification necessary to the impulses transmitted through the summation and difference channels as indicated above depends upon a number of factors, including the relative spacing of the microphones and of the loud speakers, and the size and positioning of the screen. It can be shown that for low frequencies a the degree of modification required in the difference channel as compared with the 75 modification in the summation channel is given by :-

$$\mathbf{K} = \frac{2v}{j\omega} \cdot \frac{y}{\theta k} \cdot \frac{s}{x}$$

where

- v = velocity of sound.
- y = fraction of half picture film width which the image of the sound source is off centre.
- θ = angle of obliquity, in radians, of the source from the median plane 85 between the microphones,
- k = effective distance apart of the microphones.
- s = width of screen of theatre.
- x = distance apart of loud speakers -90 in theatre.

This expression in effect gives the impedance of the shunt capacity f in the difference channel in terms of the resistance i in the summation channel. It 95 holds for all frequencies where k is small compared to the wavelength, and is based on the assumption that the θ is small and that x and s are small compared with the distance of the listener from the screen 100 and loud speakers.

The portion $\frac{y}{\theta k}$ is a factor of the record-

ing, and is constant for a given arrangement if either the camera is in line with the microphones and the centre of the 105 picture, or the action does not move appreciably to or from the microphones and camera. When recording, the relative distances of camera and microphones and the focal length of the lens may be 110 adjusted to maintain this factor a constant.

The expression $\frac{s}{x}$ is a constant for the

theatre. As regards low frequencies only, the distance apart of the speakers need 11" not exceed the screen width, but should certainly not be closer than 70 percent. of the screen width. The closer the loud speakers the greater the necessary power handling capacity, but the less the 120 troubles introduced by formation of stationary waves.

For the high frequencies no definite expression can easily be obtained, and the modification, if any, used will probably 125

have to be gauged empirically by trial and error.

The arguments and formula given above are based on a direct wave analysis and 5 may have to be considerably modified in

- order to allow for reflection of other acoustic effects. It is preferred therefore to introduce the modifications it is proposed to employ, at the theatre since all factors
- 10 will then enter into consideration. It will be clear that, as indicated above, the modifying networks and channel arrangements may be employed between the microphones and the film during record-
- 15 ing, or between the record and the loud speakers during reproduction, and the latter course, in addition to allowing of adjustment of the arrangements to suit the particular theatre as indicated above,
- 20 has the additional advantage that the sound film can be reproduced by a single reproducing head or channel if, for example, one of the dual arrangements breaks down, or in a theatre which, having one installa-
- 25 tion, does not wish to go to the expense of installing a second apparatus. In order to employ successfully a

system of the kind described above it is necessary to carry out preliminary experi-30 ments to determine the most suitable value of modification to be employed for

- each recording, and it is also necessary to standardise various factors entering into every recording. In the preliminary 35 experiments, before recording, volume indicator measurements may be made with
- a standard sound source placed at the extremes of the "set", i.e. the space within which recording is to be effected, 40 and from these the proposed modifying
- network laid out. A further experiment may also be effected to standardise phase angles on the film. At the theatre a simple adjustment may be provided to
- 45 check and balance the input to the two channels, a length of test film being used for this purpose. It will thus be seen that the total theatre equipment necessary is very simple and consists in a transmission medifier for the purpose.
- 50 modifier (comprising two or four transformers, for example, artificial line resistances and the control network, which may be no more than a condenser and a resistance) and two normal sound-repro-
- 55 ducing heads or pick-ups, or one specially designed head or pick-up adapted to separate the two recordings to two complete reproducing channels. There is no reason why the second channel used 60 should not be the "stand-by" channel
- 60 should not be the stant-by channel now often installed for safety since if, as indicated above, one of the channels breaks down reproduction may be continued without serious consequences on the
- 35 other channel only.

In connection with the standardisation indicated above, while the binaural "transfer" frequency (from phase- to intensity-discrimination) need have no definite significance in recording, since it 70 is a function of the human brain, it is nevertheless necessary to fix a change-over frequency from high- to low-frequency working for recording, since this fre-quency fixes the values of the elements 75 in the modifier and thus the form of modification to be used, the distance apart of the microphones and the form of baffle between them. Any convenient frequency may be chosen as standard after 80 experience has decided which is most suitable. Instead of standardising it may be possible from the preliminary experiments to allow electrically for variation of microphone positions and/or of micro-85 phone spacing (although the latter would be extremely difficult) and it must be understood that this arrangement falls within the scope of the invention.

The above analysis is based upon con-90 siderations which take no account of sound reflections or interference during reproduction. The reflected sound waves which arise during recording will be reproduced with a directional sense and will 95 sound more natural than they would with a non-directional reproducing system. If difficulties arise in reproduction they may be overcome by employing a second pair of loud speakers differently spaced and hav- 100 ing a different modifying network from the first pair: or a row of speakers may be used with a composite, progressive modifying network to supply them : or the two speakers may be placed comparatively 105 close together.

In this last arrangement the sense of direction of the apparent sound source will only be conveyed to a listener for the full frequency range for positions 110 lying between the loud speakers; but if it is desired to convey the impression that the sound source has moved to a position beyond the space between the loud speakers the modifying networks may be 115 arranged to reverse the phase of that loud speaker remote from which the source is desired to appear, and this will suffice to convey the desired impression for the low frequency sounds. With this arrange- 126 ment of loud speakers close together, however, it would not be possible to effect a similar illusion in connection with high frequencies.

The system so far described employs to 125 receive the sound waves two nondirectional microphones, e.g. pressure microphones. Directionally sensitive microphones may also be employed spaced a small distance apart, the outputs being 130 modified as indicated so that the relative outputs of the loud speakers are controlled both by differences in phase and differences in magnitude of the microphone outputs. Such directionally sensitive microphones may be, but are not necessarily, of the type known as velocity microphones, and preferably provided with movable conductor elements so light 10 as to move substantially as the surrounding air.

Velocity or moving conductor microphones (e.g. moving strip microphones) are very suitable for any system accord-

- 15 ing to the invention and in addition to use with circuit arrangements described above: they may also be employed with various alterations in the circuits. These microphones give a response varying as
- 20 the cosine of the angle of incidence of the sound relative to the direction of normal or optimum incidence, and they therefores have the advantage that a certain degree of loud speaker output separation may
 25 be obtained without phase-conversion or like network modifications.

Three general arrangements employing velocity microphones are possible, and in all cases the microphones are placed as 30 near together as possible instead of being spaced as artificial ears, as in the case of pressure microphones.

 Two velocity microphones are placed one with its axis of maximum response
 directly facing in the direction of the centre of the scene, and the other with its axis at right angles to that direction. Both moving strips are in line, ind arranged so that this line is vertical,
 we treas the sound source moves in a horizontal plane. A performer speaking from the middle of the scene will affect only the face-on microphone, but if he moves to one side both microphones will

- 45 provide outputs, while if he moves the other way similar outputs are provided but the phase of the edge-on microphone is reversed. Since the microphones are close together no phase differences are 50 experienced between them and if their
 - outputs are summed and differenced after a suitable amount of relative amplification the two final channels differ in magnitude in the correct manner for operating the 5 loud speakers to give the desired direc-
- 55 loud speakers to give the desired directional effect. Such sum and difference arrangement differs from the modifying network employed with pressure microphones in that the pressure type provide
 60 phase differences (whereby direction is
- determined) which have to be converted, whereas with the velocity type the edgeon microphone provides an output proportional to the obliquity of the source. 65 A suitable modifying arrangement for

this form of the invention is shown in Figure 6. This is substantially identical with that shown in Figure 5 except that the shunt condenser f and resistance k in series, and the shunt resistance i are replaced by shunt resistances l m which are preferably variable as shown. These lines therefore form artificial attenuators and by altering their relative attenuation the intensity differences in the two lines corresponding to a given obliquity of sound is controlled.

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(2) Two velocity microphones or microphone elements, may be placed with their axes perpendicular to one another and . 3 each axis at 45° to the direction of the centre of the screen. This arrangement is represented diagrammatically in Figure 2 wherein n and o represent two velocity, or directionally sensitive microphones one above the other arranged perpendicular to one another and at equal angles at 45° to the direction of the centre of the field from which sound is to be received. 1, will be clear that movement of the sound A source a laterally to a position p removed from the centre of the field will result in the sound waves striking o at a more acute angle than they strike n and differences in the microphone outputs will result. The microphones are sufficiently close together to render phase differences of the incident sound negligible and the output amplitudes therefore differ approximately proportionally to the obliquity of the 160 incident sound. They may therefore be amplified similarly, and supplied directly to the loud speakers to which they will give the correct amplitude differences for the desired directional effect provided the 10relationship between the various dimensions of the recording and reproducing "lay-outs" are correct. If it is desired to accommodate any differences between the " lay-outs " the outputs may be modi- 116 fied by networks, in the manner described, suitably to increase or decrease the differences between them. An arrangement such as shown in Figure 6 is suitable for this purpose, and such an 113 arrangement may of course also be employed even if the lay-out is correct if it is desired for any reason to control or modify the amplitude differences of the loud speaker outputs. 429

(3) Two microphones may be arranged with the two axes lying symmetrically to the direction of the centre of the field and with an angle between them of say θ degrees, so that sound from a performer 125

at the centre subtends an angle of $\frac{0}{2}$

degrees to each microphone. If θ is small a small movement of the performer to one side is sufficient to make one microphone

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"edge-on" and to reduce its output to zero, while if θ is large a large movement of the performer is necessary to do this. By making θ adjustable different "lay-5 outs" may be accommodated without the modification indicated under (2) and it

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will be clear also that this provides a method of directional sound transmitting, recording and reproduction which avoids 10 the necessity of combining and reseparating the two channels.

The microphone elements in any of the above cases may be enclosed in a single casing if desired for convenience, and may 15 also be positioned in a single magnetic

system common to both. Two velocity microphones set in line with one another and with their axes of maximum response symmetrically inclined 20 to the direction of the centre line of the scene, may, if placed one above the other, be employed also to provide significance of vertical as well as horizontal movement of the sound source in a plane perpen-25 dicular to the axis of maximum response of the microphone system. Such vertical displacement of the source will in this arrangement give phase differences to the outputs while lateral displacement gives 30 amplitude differences, and these can be separated, the phase differences converted to intensity differences by modifying networks, as described, and the resulting impulses employed to operate four or 35 more loud speakers distributed round the The transmission in such a screen.

system occupies only two channels (one leading from each microphone) up to a point in the system where each of these 40 channels is divided into two parallel

- channels thus providing four channels in all at this point. Two channels, one from each parallel pair of these divided channels, are connected to one modifying 45 network adapted to deal with phase
- differences, and the other two channels, one from each pair, connected to another modifying network adapted to augment intensity differences. Each modifying 50 network operates a plurality of loud
- speakers providing a directional sensation in one direction, and in this manner directional senses in two directions at right angles can be obtained. It will be 55 seen that in such an arrangement the transmission and/or recording (which is the most expensive and difficult operation of the system) may be effected over only two channels although directional sensations in two perpendicular directions are subsequently obtained. A similar effect may be obtained with a plurality of pressure microphones by employing suit-

able modification previous to transmission. 65 In obtaining a complete directional

" sound picture ", i.e. both horizontal and vertical directional effects, the invention is not limited solely to the use of two microphones. A plurality may be employed and their outputs suitably col-70 lected, modified and separated to transmit suitable differences of impulses to a plurality of loud speakers. The general feature is that two transmitting channels, receiving impulses from two or more 75 microphones for example, communicate impulses which can be modified and separated to provide two directional senses at right angles to one another, the sounds whereby this is done being provided by a plurality of loud speakers. It will 80

moreover be clear that if the sound source moves away from or towards the microphones the overall intensity of the combined loud speaker propagations will vary 85 and thus provide indication of the position of the source along that axis. Full threedimensional location of the source is thus obtained by this arrangement.

It will be seen that while with pressure 90 microphones it is preferred to transmit phase differences rather than amplitude differences and convert from one to the other as late as possible prior to reproduction, with velocity microphones it is 95 more convenient to tranmit the two channels in phase but at different amplitudes, the only modification then necessary being an increase or decrease of the amplitude differences should the reproducing "lay-out" differ from the recording "lay-out" or should more than two loud speaker positions be used.

There is a simple method by which modifications for increase or decrease of 105 differences between channels may be effected if no conversion of phase differences into amplitude differences is required. The method is particularly useful for the operation of more than two 110 loud speakers, and is also useful for working into high impedances such as the grid impedance of a thermionic valve. The arrangement is shown diagrammatically in Figure 7. If the transmission is 115 effected in the form of two channels r sof similar phase but different amplitudes, an alteration of these amplitude amplitude differences may be effected by connecting one wire of each channel r and s together 120 at t and connecting a choke u between the other two wires of the two channels. The outgoing channels v and w whose difference is to be a modification of the original difference, are connected by one 125 wire each to the common point t of the original channels, and by their otherwires to tappings along the choke u. If the differences are to be increased, the tappings at which the output channels are 130

connected lie outside the tappings to which the input channels are connected, so that the choke operates in effect as an auto - transformer amplifying the 5 difference voltages. Similarly, for a reduction of differences, the output channels are tapped intermediately between the two input channels. Modifications of this arrangement in which the devices are 10 balanced about earth, etc. may be arranged, but the chief advantage is that the modification is varied entirely bv altering tappings along a transformer or choke, and that no great power loss is 15 involved.

This arrangement of a choke or transformer is well suited to working a number of loud speakers for binaural reproduction. In this case, the two outputs from 20 power valves are fitted to a choke such as

 \hat{u} along which the loud speakers are tapped. The position of the loud speaker tappings can be adjusted to suit their relative positions, and it can be arranged 25 that the valves are working into their best impedances. Transformers may be used to

ensure the speakers taking their correct fraction of the output.

While, in connection with the above 30 described systems, it is suggested that when it is desired to record the sounds for subsequent reproduction this may be done upon a film, the invention is not limited to that medium since the recording 35 may if desired be effected on discs or cylinders of suitable material. In carrying out the invention in this manuer the two channels may if desired be recorded in separate grooves but it is preferred that

- 40 they be recorded in the same groove having a hill and dale and also a lateral cut movement. For the purposes of television previous proposals have been made whereby a wax disc has a sound record
- 45 as a hill and dale cut and a picture record as a laterally cut V-shaped groove at the bottom of the hill and dale groove, or vice versa. Such records appear unsuited for separate and distinct sound recordings

50 since undoubtedly considerable cross-talk between the two recordings would occur. They can however be used for two channels of the kind contemplated in the present invention, one being only slightly

- 55 different from the other, since a certain amount of cross-talk in this case does not matter, or can be allowed for. Furthermore, the records now proposed are distinguished from those previously known in
- 60 that both channels may be recorded as separate cuts in one groove and may be recorded by a single recording tool (either of moving iron or moving coil type) and be reproduced therefrom by a single 65 reproducing device or pick-up.

If the two channels being recorded are directly picked up from two microphones. or are intended to work unmodified into two speakers, that is with intensities and qualities similar to those of the original sounds received, it is preferred not to cut one track as lateral cut and the other as kill and dale, but to cut them as two tracks whose movement axes lie at 45° to the wax surface, or at some other convenient angle dependent on the relative available intensities from lateral cut and hill and dale respectively. If, however, the two channels recorded are such as summation and difference channels, it is preferred to separate them completely into pure hill and dale and pure lateral cut, i.e. to make the recording axes normal and tangential to the wax surface.

The result in the two above suggested cases is very similar since channels recorded at 45° to the wax surface give their sum and difference as the effective lateral and hill and dale amplitudes.

It will be appreciated that a record, \$ cut as a combined hill and dale and lateral, may be reproduced if desired as two skew direction cuts, the basic principle being that the groove has amplitude in any direction in the plane 81: at right angles to the direction of wax movement, and the recording and reproducing directions may be chosen as any pair of axes lines, not necessarily at right angles, in this plane.

It would appear that for such a record, a material other than that now used for lateral cut records, would be desirable, and a material of the nature of cellulose acetate is indicated.

The track section is preferably adapted to work with a sapphire and have a sufficiently fine angle to give lateral as well as vertical control to the sapphire.

The recorder whereby both channels 410 may be cut by a single tool on the same groove may take various forms, the underlying feature being that a light stylus is pulled into two directions at right angles to one another and each preferably at 45° 115 to the wax surface.

Figure 8 shows schematically a recorder of this kind suitable for producing records having complex cuts. 1 and 2 represent the driving elements of two recorders 120 normally adapted for cutting lateral cut These driving elements drive records. arms 3 and 4 about axes at right angles to the plane of the paper within 1 and 2. The ends of these arms are connected by 125 ligaments 5 and 6 to the end of a reed 7 which extends backwards along an axis perpendicular to the paper to supports This reed carries a cutting not shown. sapphire 8. Movements of the recording 4.30

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arms 3 and 4 produce movements in the end of the reed 7. Thus, currents in movement 1 will cause the reed 7 to move along an axis approximately 45° to the

- 5 vertical rising from left to right across the figure. Similarly, currents in movement 2 will produce movement of the reed 7 in an axis at right angles to the former axis, while currents in both move-10 ments will of course result in vertical
- movement of the reed. Another such form of recorder shown
 - in Figure 9, representing a moving iron recorder, may consist in a short reed 9
- '5 mounted close above and parallel with the wax track and carrying the cutting sapphire 8. This reed 9 may extend backwards perpendicularly to the paper to supports (not shown) which join the top
- 20 of a laminated pole system 10 to complete a polarising magnetic system therewith. The two laminated arms of the pole piece 10 extend down towards the free end of the reed 9. These arms form two poles
 25 adjacent to a square portion of the reed at its free end, each pole being adapted
- to pull the reed in a direction at 45° to the wax surface. The reed may be suitably damped, e.g. by a rubber line, and **30** have a resonant frequency at the top of, or
- above, the working range. The two pole pieces may be wound with speech coils, and the energisation of one of these moves the sapphire in an upward direction at 452 to the war surface. The terminals 15
- 35 45° to the wax surface. The terminals 15 of one channel are connected to main winding 12 and compensating winding 11. The terminals 16 of the other channel are connected to main winding 14 and
- 40 compensating winding 13. Current in either channel will pull the reed towards the pole carrying the main winding, the purpose of the compensating winding being to prevent movement of the reed
- 45 away from the other pole due to the flux drawn away from this pole by the main winding. With the winding shown, currents in either channel will cause the reed to cut a track at approximately 45°
- 50 to the vertical. By a suitable rearrangement of windings, or by a suitable transformer connection between the channels and the terminals of the recorder as shown, any other movement axes may
 55 be obtained. Thus for example the tool
- 55 be obtained. Thus for example the tool may have one movement by torsion of its supporting reed and another by flexure thereof.
- An alternative moving coil design which 60 may employ electromagnetic damping may consist of a moving member in the shape of a T as shown in Figure 10. The recorder sapphire 8 is supported on a light T member 17, which is supported at 18 by 65 elastic means such that it may rotate about

this point, and may also translate vertically, though it is resistant to horizontal movements in the plane of the paper. The device is driven by moving coils, e.g. speech coils, 19 and 20 which are freely located and immersed in the 70 steady magnetic field provided in annular gaps in a magnetic system, not shown. Current in one of the moving coils tends to both rotate and translate the device so .75 that the sapphire 8 moves along an axis at approximately 45° to the vertical. The movement of this device may be damped and equalised along the lines described in British Patent Specification No. 350,998. 80 As before any required axes of movement may be obtained by suitable interconnection of the two driving coils. Such a movement preferably has the same natural frequency for both rotation and transla-85 tion. Further the distribution of mass is preferably such that a small instantaneous force applied at one coil produces no movement at the other.

Figure 11 shows another form of 90 recorder similar in principle to the one shown in Figure 10 except that a moving iron drive is employed. The member 17 moving about axis 18 is constructed of magnetic material, or has a magnetic upper portion. The "E" shaped member 21 is polarised either by being partially permanently magnetised, or having a magnetising winding on it, so that the central pole is of opposite polarity to the 100 two outer poles. Speech windings on the outer poles are brought out to terminals 15 and 16 to which the two channels are connected.

In all the devices described above, the 105 angles of the axes defining the movements of the sapphire can be altered by suitably connecting the speech windings; for instance, axes which are normally inclined at 45° to the wax surface can be converted into pure hill and dale and lateral cut axes by arranging that the speech windings are in series aiding for one channel and opposing for the other channel. In like manner any axis conversion can be 115 effected by suitably combining the channels through transformers.

In designing an electric pick-up to reproduce both channels care must be taken that the inertia is kept as low as 120 possible, and with this in mind a very light replica of any of the above described recorders may be employed. Preferably, a moving system in the form of a T following the lines of the moving iron 125 recorder shown in Figure 11 is employed as best suited for the purpose. Since the fundamental resonant frequency of a pickup appears to be of no critical importance as regards its characteristic, it may not 130

be necessary to adjust the resonant frequency in the two modes to the same value, which would simplify the design. Adjustments for sensitivity in the two modes may be made by suitably connect-5 ing coils wound on the two limbs of the magnetic circuits. As in the recorder design the distribution of mass in the reproducer is preferably such that forces 10 producing motion in one direction (e.g. lateral movements) leave it substantially undisturbed in its reproduction by motions in another direction (e.g. hill-and-dale). A good binaural effect may be obtained 15 by giving directional significance to only a limited range of frequencies. For example, although good reproduction requires the transmission of all frequencies up to, say, 10,000 c.p.s. yet a good direc-20 tional effect is obtained from frequencies up to, say, 3,000 c.p.s. This would assist disc recording of the binaural impulses since the lateral cut which represents the sum of the two channels to the speakers 25 might have a frequency range extending to 10,000 c.p.s. whereas the hill-and-dale cut need transmit frequencies no higher than 3,000 c.p.s. This would consider-ably simplify the design of the recorders and pick-ups in that low inertias would 30 only be required for the lateral cut and design would thus be greatly simplified. These frequencies are given merely by way of example, and are not necessarily 35 the optimum frequencies for design of this character, which will be determined by other considerations. In transmitting the two channels indicated in the various systems above

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- 40 described, instead of employing line transmission, radio transmission may Each employed. desired be if channel may be separately transmitted or preferably the two channels may be '45 sent as different modulations of the same carrier wave. Thus one channel may be transmitted as an amplitude modulation and the other as a phase or frequency modulation of the same carrier wave. 50 Alternatively the two channels may be transmitted as amplitude modulations of different carrier waves which are 90°
- out of phase, the two waves being radiated from the same aerial in combination as a 55 single wave propagation. Various systems
- for the transmission and reception of duplex radio signals along these lines are known and any one of such or similar arrangements may be used in connection 60 with the invention described herein
- according to its applicability or convenience in the circumstances under consideration. It must be understood that with such a system of duplex radiation, it
- 65 is possible, if desired, to perform one of

the summing and differencing processes in the radio link. For example, by demodulation at the receiving end with two carrier waves 90° out of phase, which carrier waves are 45° out of phase with 70 the original modulating carriers, the resultant low frequency channels are the sums and differences of the original low frequency channels at the transmitter.

The hereindescribed system while being 75 especially applicable to talking pictures is not innited to such use. It may be employed in recording sound quite inde-pendently of any sist pendently of any picture effects and in this connection (as well as when used in 80 cinematograph work) it seems probable that the binaural effect introduced will be found to improve the acoustic properties of recording studios and to save any drastic acoustic treatment thereof 85 while providing much more realistic and satisfactory records for reproduction. Furthermore, the system may clearly be employed when the microphone outputs are led to the loud speakers instead first 90 of being recorded, and such an arrangement may for example be employed in public address systems in which direc-tional sound effects are desired. In general the invention is applicable in all 95 cases where it is desired to give directional effects to emitted sound. Also in all cases, both when the impulses are fed to the loud speakers without recording and when they are recorded for subsequent re- 100 production the total modification and/or interaction of the channels may be accomplished in more than one stage. For example, using pressure microphones, the low frequency phase differences may be 105 augmented, the medium frequency phase differences converted to amplitude differences, and the high frequency amplitude differences augmented in a first stage of modification; the low frequency phase 110 differences may then be converted to amplitude differences in a later stage of modification. One or both of these stages may occur either before or after the sound has been recorded. In this manner the 115 very small low frequency phase differences are augmented before they are amplified, so avoiding troubles due to small low frequency phase shifts in amplifiers.

Moreover, the various devices employed 120 for carrying the invention into effect must be understood not to be limited to their use with the other devices in the systems also hereindescribed since clearly many parts, such, for example, as the 125 dual track record prepared by a single cutter, and the multi-strip directiondetecting microphone, are clearly of wide use in such systems separately from one another. Such uses in binaural systems 130

as herein described fall within the scope of this invention.

- It must finally be understood that the invention is not restricted solely to the 5 details of arrangements of the forms of the invention described above since various modifications may be introduced in order to carry the invention into effect under different conditions and require-
- 10 ments which have to be fulfilled without departing in any way from the scope covered thereby.

Having now particularly described and ascertained the nature of our said inven-

15 tion and in what manner the same is to be performed, we declare that what we claim is :---

1. A system of sound transmission wherein the sound is picked up by a

20 plurality of microphone elements and reproduced by a plurality of loud speakers, comprising two or more directionally sensitive microphones and/or an arrangement of elements in the transmission 25 circuit or circuits whereby the relative loudness of the loudspeakers is made dependent upon the direction from which the sounds

arrive at the microphones.

2. A system of sound transmission 30 wherein the sound is received by two or more microphones, wherein at low tre-quencies difference in the phase of sound pressure at the microphones is reproduced as difference in volume at the loud 35 speakers.

3. A system of sound transmission, in which the original sound is detected by two cr more microphones of a type such as velocity microphones whose sensitivity

'40 varies with the direction of incident sound, and in which the dependence of the relative responses of the microphones on the direction of an incident sound wave is used to control the relative volumes of 45 sound emitted by two or more loud speakers.

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4. A system of sound transmission wherein two or more microphones are used to detect the original sound, and both the 50 relative phase and volume of the output of the two microphones are used to control, according to the direction of

incidence of the original sound wave, the relative output volumes of two or more 55 loud speakers.

5. A system according to any of Claims 1-4 in which two or more channels are combined and separated into other channels so that the resultant 60 channels, though not similar to the former channels, are modifications of them conveying the same directional intelligence in another form.

6. A system of sound transmission. .65 wherein impulses from two microphones transmitted over individual channels are adapted to interact whereby two sets of impulses are further transmitted consisting in half the sum and half the difference respectively of the original im-70 pulses, said impulses being thereafter modified to control the relative loudness of loud speakers whereby the sound is to be reproduced.

7. A system as claimed in Claim 6 75. wherein after modification the two sets of impulses are treated by a repetition of the sum and difference process initially effected.

8. A system as claimed in Claim 6 or 80wherein after the initial impulses have 7 been translated to sum and difference impulses modification is effected in each sum and difference channel by attenuator networks and/or phase modifying arrange-85. ments.

9. A system as claimed in Claim 8 wherein modification of the impulses is effected by plain shunt elements, e.g. resistances and/or condensers, which may 90 be variable in value.

10. A system according to any of Claims 5-9 wherein for part of the frequency range phase differences in the original channels are converted to ampli-95 tude differences in the resultant channels.

11. A system according to any of Claims 5-10 wherein over all or part of the frequency range the differences between the channels are augmented or 100 reduced.

12. A system according to any preceding claim comprising two separate microphones arranged apart by a short distance, approximately equal, for example, to the 105 separation of the human ears.

13. A system according to Claim 12 comprising two pressure microphones between which a baffle is provided.

14. A system according to any of 110 Claims 2 or 4-12 comprising directionally sensitive microphones.

15. A system of sound transmission wherein the sound is picked up by two directionally sensitive microphones which 115 are so spaced and/or with their axes of maximum sensitivity so directed relative to one another and to the sound source, that the relative loudness of loud speakers which reproduce the impulses is controlled 120 by the direction from which the sound reaches the microphones.

16. A system as claimed in any of Claims 1-11, 14 or 15 comprising two velocity microphones or microphone 125 elements placed in close juxtaposition with their axes of maximum sensitivity pointing in different directions.

17. A system as claimed in any of Claims 1-12 or 14-16 comprising 130 velocity microphones or microphone elements in the form of a conductor so light as to move substantially as the surrounding air.

5 18. A system as claimed in any of Claims 1—12 or 14—17 wherein a plurality, e.g. two, velocity microphone elements are built into a single container with a common magnetic system, or 10 separate magnetic systems.

19. A system as claimed in any of Claims 1-12 or 14-18 comprising two velocity microphones, one with its element perpendicular to the direction of the 15 centre of the "sound field" and the

- 15 centre of the "sound field" and the other with its element in line with said direction, both elements lying longitudinally in line, and at right angles to the plane in which the sound source moves.
- 20. 20. A system as claimed in any of Claims 1—12 or 14—18 wherein two velocity microphones lie with their elements at equal angles (e.g. each at 45°) to the direction of the centre of the sound
 25 field.

21. A system as claimed in any of Claims 1-12, 14-18 or 20 comprising two velocity microphone elements the angle between which (and hence the angle 30 of each relative to the centre of the "sound field") is adjustable.

22. A system as claimed in any of Claims 15-21 wherein the directionally sensitive microphones are so arranged and
35 directed as to provide impulses whereby the desired relative loudnesses of the loud speakers are obtained, said impulses being transmitted to the loud speakers without

- modification or interaction.
 23. A system as claimed in any of Claims 15-21 wherein the, impulses generated by the directionally sensitive microphones are modified (e.g. by attenuator networks in sum and difference channels)
 25 before being reproduced by the load
 - speakers. 24. A system as claimed in Claim 23 wherein modification is effected by a common choke inserted between two
- 50 microphones and two loud speakers, four leads (one from each microphone and each loud speaker) being connected together while the other lead from each member is movably connected to tappings on the 55 choke.
 - 25. A system as claimed in any of Claims 1-21, 23 or 24 wherein the modification of the impulses is effected in two or more stages.
- 60 26. A system as claimed in any preceding claim wherein the transmitted impulses are photographically recorded upon separate film sound tracks, preferably adjacent to one another, either track being
- 65 either of the variable width, or variable

density form.

27. A system as claimed in any of Claims 1-25 wherein a record of two sets of impulses is located upon a single film track in the form of a combined variable 70 width and variable density recording.

-28. A system as claimed in any of Claims 1-25 wherein the impulses are recorded upon discs or cylinders of wax or like suitable material.

29. A system as claimed in any of Claims 1-25 or 28 wherein the two sets of impulses are recorded upon the same cylinder or disc.

30. A system as claimed in Claim 29 80 wherein two sets of impulses are mechanically recorded in the same groove.

31. A system as claimed in Claim 29 or 30 wherein one record is a lateral cut and the other a hill-and-dale cut in a 85 single groove.

32. A system as claimed in any of Claims 28-31 wherein the recordings are effected simultaneously.

33. A system as claimed in any of **90** Claims 28—32 wherein the recordings are effected by a single cutting tool.

34. A system as claimed in Claim 33 wherein the cutting tool is capable of controlled movement in all directions in a plane perpendicular to the direction of movement of the wax.

35. A system as claimed in Claim 33 or 34 wherein the cut of the recording tool is in form a combination of lateral 180 and hill-and-dale cuts, or equivalent to that form.

36. A system as claimed in any of Claims 28—35, wherein one channel is recorded as a cut in a direction at an 105 angle to the normal to the wax and the other channel is recorded as a cut at the same angle to the normal to the wax but on the other hand relative to the groove.

37. A system as claimed in any of 110 Claims 26-36, wherein the desired modification of the two channels is wholly effected either before recording or after reproduction from the record, or is partially effected in each stage. 115

38. A sound reproducing system wherein the sounds are reproduced without modification from one or more sound records prepared by a system according to any preceding claim. 120

39. Microphone arrangements for a system according to any preceding claim comprising a plurality of directionally sensitive elements arranged with a common magnetic system, or separate 125 magnetic systems, in a common casing or container, the axes of maximum sensitivity of the elements being arranged at an angle to one another, the elements being connected to separate transmission 130

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chaunels whereby the impulses are separately transmitted from the elements. 40. Microphone arrangements as claimed in Claim 39, wherein the angle 5 between the elements is adjustable.

41. A system according to any of Claims 28-37, embodying a sound recorder comprising an operating movement adapted to respond to both channels 10 of impulses and to cut records of both simultaneously.

42. A system embodying a sound recorder as claimed in Claim 41 comprising a single cutting tool adapted to operate 15 in a single groove.

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43. A system embodying a sound recorder as claimed in Claim 41 or 42 adapted to effect a different kind of recording cut (e.g. lateral or hill-and-dale) for 20 each of the channels.

44. A system embodying a sound recorder as claimed in Claim 41 or 42 adapted to respond in similar manner to, and effect cuts of similar form for, each 25 channel, but in opposite sense relative to

the groove. 45. A system embodying a sound recorder as claimed in any of Claims 41-44 comprising a cutting tool capable of 30 controlled movement in all directions in a plane perpendicular to the direction of

movement of the wax.

46. A system embodying a sound recorder as claimed in any of Claims 41-

35 45 comprising a cutting tool the movements of which in two directions, perpendicular or at an angle to one another, are separately controlled by the driving arms of separate recording elements.

47. A system embodying a soun recorder as claimed in any of Claims 41a sound 40 45 comprising a cutting tool carried upon a flexible reed adapted to be moved in either of two directions, perpendicular or

45 at an angle to one another; or to be subjected to a resultant movement equivalent to the combination of such motions in both directions.

48. A system embodying a sound 50 recorder as claimed in Claim 47 wherein movements of the reed are effected by electromagnetic forces imposed by adjacent poles of a co-operating magnetic system excited by the impulses to be 55 recorded.

49. A system embodying a sound recorder as claimed in Claim 48 wherein compensating coils are wound on the magnetic system in addition to the excit-60 ing speech coils in order to neutralise

effects upon one pole of impulses in the speech coil of the other pole.

50. A system embodying a soun recorder as claimed in any of Claims 41a sound **5**5 45 comprising a cutting tool assembly adapted to have one movement by torsion of its supporting reed and another by flexure thereof.

51. A system embodying a sound recorder as claimed in Claim 50 wherein 70 the cutting cool assembly is driven by moving coil drives, comprising speech coils attached thereto freely immersed in a steady magnetic field.

52. A reproducer for a transmitting system as claimed in any of Claims 1-75 38, comprising elements of small weight and inertia but otherwise substantially identical in form and arrangement with those of a recorder as claimed in any of 80 Claims 41-51, the cutting tool therein being replaced by a stylus whereby electrical vibrations are produced in the magnetic windings by vibrations imparted 85 to the movable reed or like movable armature.

53. A system as claimed in Claim 41 embodying a sound recording or sound reproducing device substantially as represented in Figure 9.

54. A system as claimed in Claim 41 embodying a sound recording or sound reproducing device substantially as represented in Figure 10.

55. A system as claimed in Claim 41 embodying a sound recording or sound 95 reproducing device substantially as represented in Figure 11.

56. A sound record prepared by a system as claimed in any of Claims 1-38 100 or 41-51.

57. A sound record comprising in one groove two substantially separate records of sound which emanate from the same source, which sounds are picked up by 105 directionally sensitive devices and/or are subjected to modifications by elements in the recording circuit, in such a manner that when the records are reproduced, one in one loud speaker and the other in 110 another loud speaker, the intensities of the sounds simultaneously propagated convey in combination a true binaural effect to the listener.

58. A sound record as claimed in Claim 115 57 comprising separate cuts of different form, or of same forms along any pair of axes in a plane perpendicular to the direction of movement of the wax, for the separate recordings. 126

59. A sound reproducing device adapted to reproduce sounds from motions in one direction (e.g. lateral movements) on a sound record prepared according to any of Claims 43-51, while remaining sub- 125 stantially undisturbed in its reproduction by motions in another direction (e.g. hilland-dale).

60. A system as claimed in any of Claims 1-39 wherein the impulses are 130

transmitted by radio telephony.

61. A system as claimed in Claim 60 wherein transmission is effected by the duplex modulation of a sing. rier 5 wave, or by radiation of a single wave formed of separately modulated components.

62. A system as claimed in any of Claims 1-39, 60 or 61 in combination 10 with means for the photographic record-

ing, or for the reproduction of pictures. 63. A sound and picture reproducing

system as claimed in Claim 62 wherein the relative volumes of the reproducing

- 15 loud speakers are so controlled as to provide apparent location of the sound origin in coincidence with the optical location of the image from which the sound is supposed to emanate.
- 20 64. A system as claimed in Claim 62 or 63 wherein the relative modifications of the two channels is determined by the dimensions and lay-out of scene to be recorded, and/or the theatre in which reproduction is presented. 25

65. A system as claimed in Claim 62, 63 or 64 wherein the relative values of the modifying networks in the two channels is defined by the formula

where the symbols have the meanings defined herein.

66. A system as claimed in any of Claims 1-39 or 60-65, or a plurality of such systems in combination as a single 35 system, adapted to provide a full directional significance to sounds emitted by a source movable in any direction in a plane-perpendicular to the axis of maximum response of the microphone system.

67. A system as claimed in Claim 66 wherein the total sound emission of all loud speakers determines the position of the sound source along the said axis of maximum response, so that full three-45 dimensional acoustic location of the sound source is obtained.

68. Systems of sound transmission substantially as described herein, with reference to the accompanying drawings.

69. Means for the transmission, recording and reproducing of sound substantially as described herein with reference to the accompanying drawings. 70. Systems for the transmission,

55 recording and reproduction of combined picture and sound effects substantially as described herein with reference to the accompanying drawings.

 $\mathbf{K} = \frac{2v}{j\omega} \cdot \frac{y}{\theta k} \cdot \frac{s}{x}$

Dated this 9th day of November, 1932. MARKS & CLERK.

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